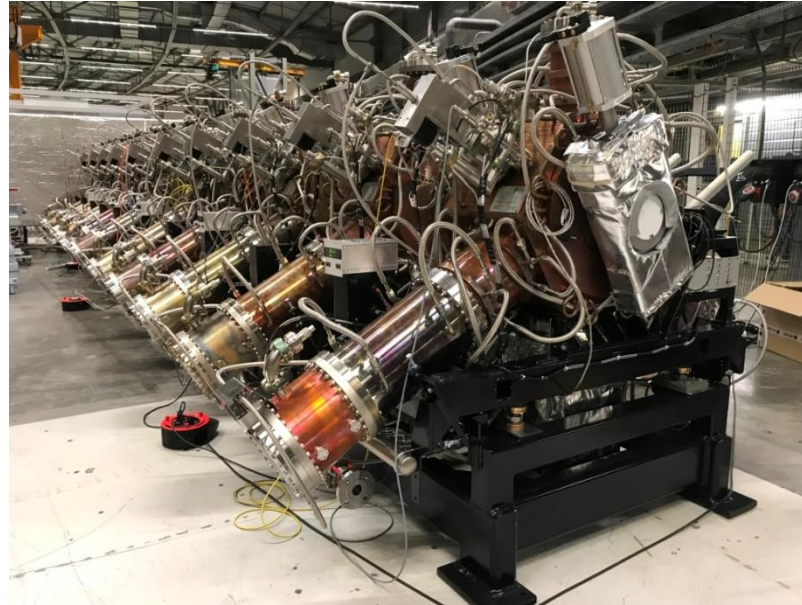


22nd ESLS RF Meeting - SOLEIL

Paris, 8-9 November 2018

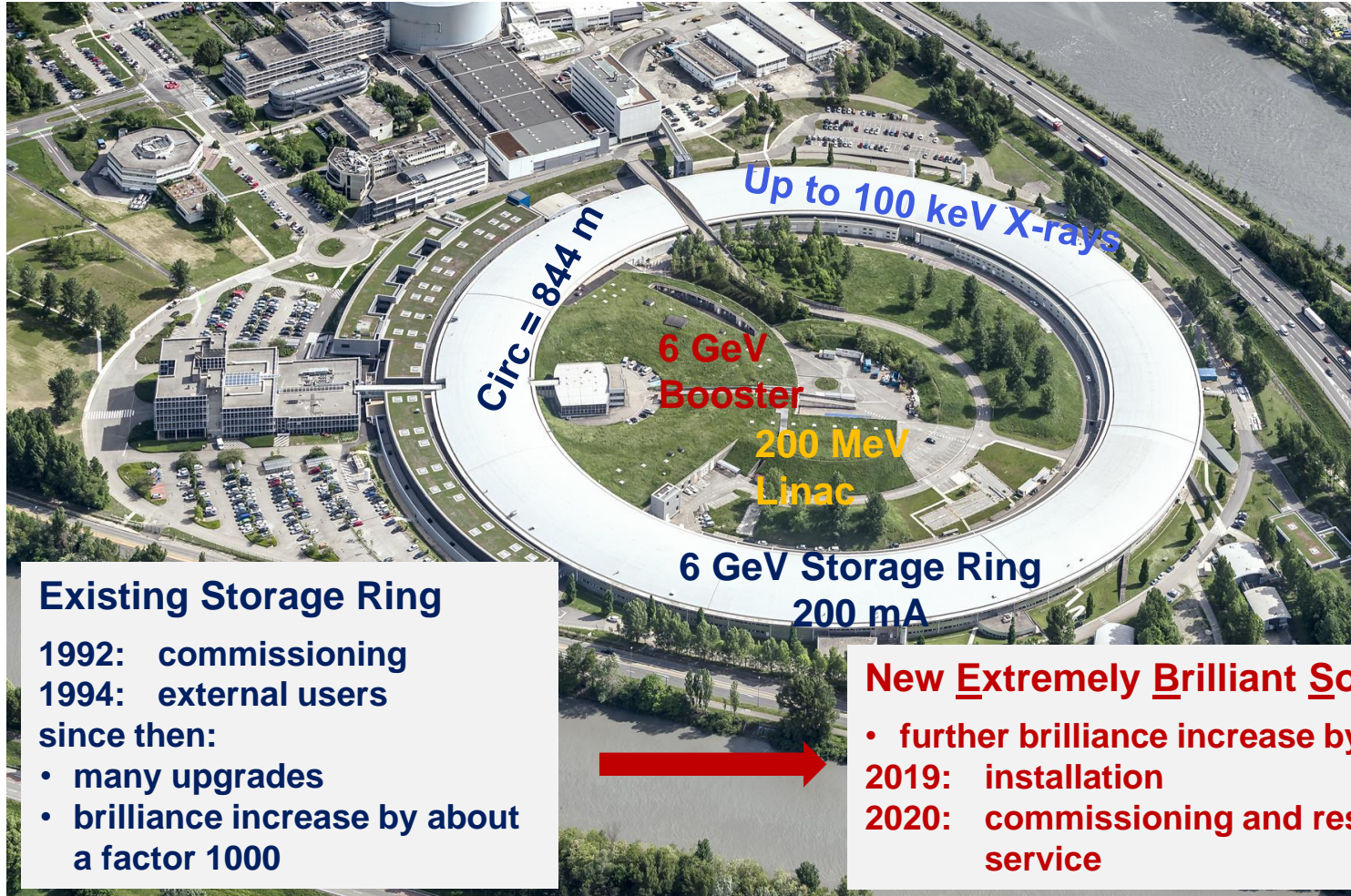
*Harmonic RF systems for ESRF-EBS
- Preliminary considerations -*

Jörn Jacob, Vincent Serrière



The European Synchrotron

ESRF: FIRST 3rd GENERATION SYNCHROTRON LIGHT SOURCE



Existing Storage Ring

1992: commissioning

1994: external users

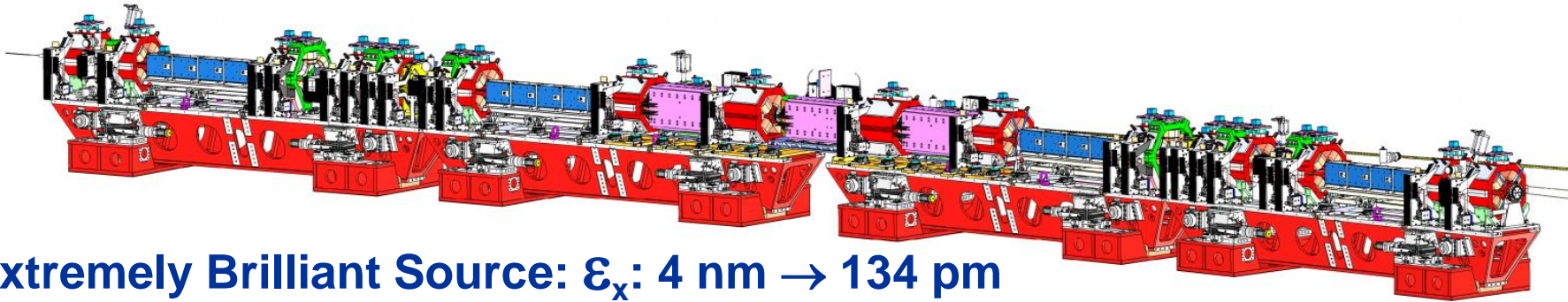
since then:

- many upgrades
- brilliance increase by about a factor 1000

New Extrremely Brilliant Source: EBS

- further brilliance increase by a factor 40
- 2019: installation
- 2020: commissioning and resume user service

RF UPGRADE FOR THE ESRF-EBS STORAGE RING



Extremely Brilliant Source: ϵ_x : 4 nm \rightarrow 134 pm



**10 December 2018: shut down existing machine
2019: Installation of new machine
2020: Commissioning EBS and Beamlines
August 2020: Back to user service mode**

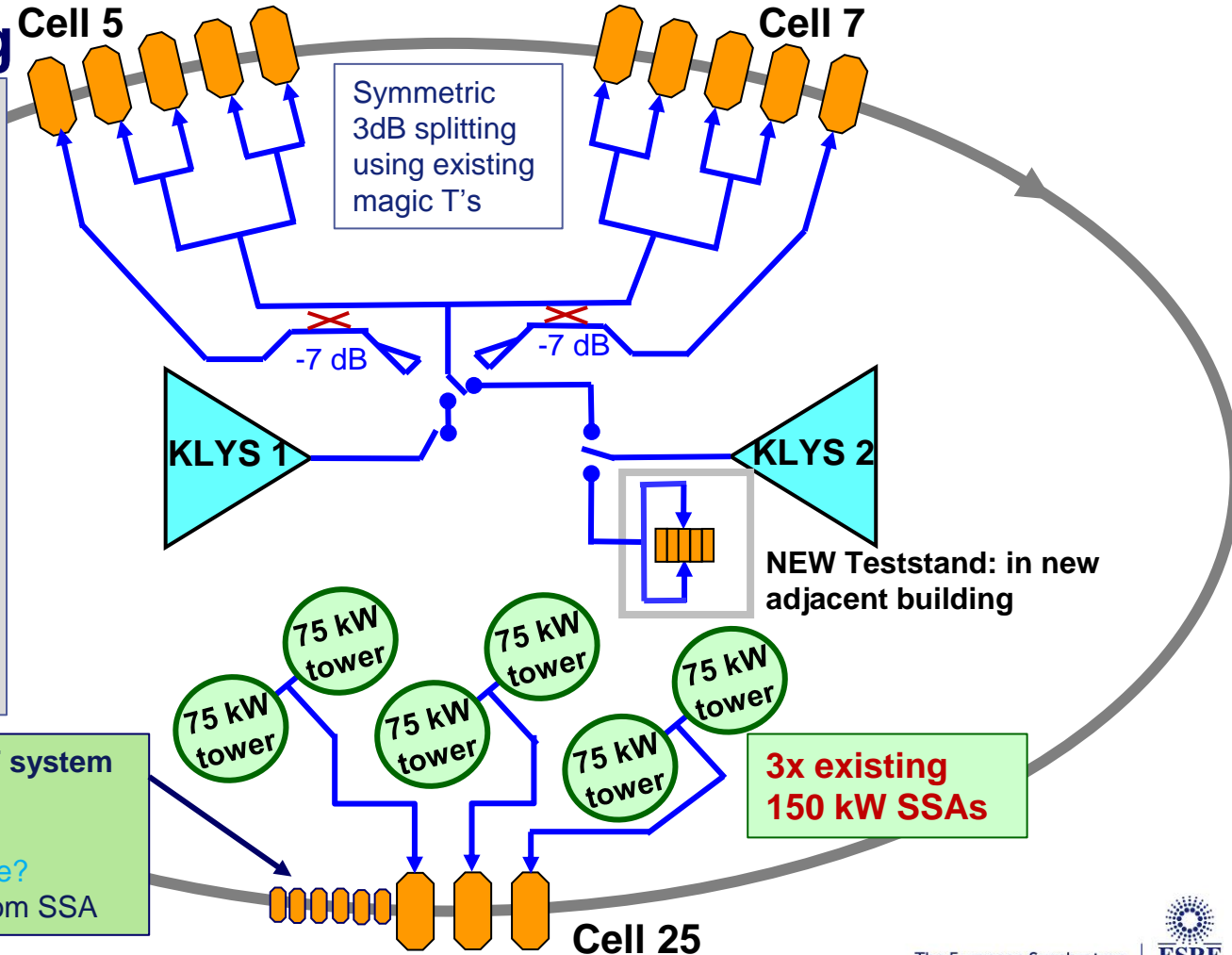
EBS Storage Ring

EBS RF upgrade:

- Remove 5 five-cell cavities
- Remove 2 prototype HOM damped cavities from cell 23
- Install 13 single cell HOM damped cavities in cells 5, 7, 25
- Suppress existing 3rd Klystron transmitter in cell 25
- Move 3 x 150 kW SSAs from cell 23 to cell 25
- Rebuild waveguide distribution system
- Rebuild control system for klystron transmitters and cavities

Space for 3rd harmonic RF system

- Still under study:
5 to 6 active NC cavities
or passive Super3HC type?
- ≈ 40 kW per NC cavity from SSA



MAIN RF PARAMETERS FOR ESRF-EBS UPGRADE

Total energy loss:

- ☞ Energy loss from dipole radiation:
- ☞ Energy loss from ID radiation:

3.2 MeV/turn

2.5 MeV/turn

0.7 MeV/turn

Maximum RF Voltage:

6.6 MV

Stored current with operational margin:

220 mA

HOM damped cavities:

- ☞ 2 of 3 prototypes on SR since 2013:
- ☞ Prototypes validated with beam up to:
- ☞ All 12 series cavities conditioned to:

0.5 MV / 90 kW (*standard operation*)

0.6 MV / 150 kW (*phased for max beam loading*)

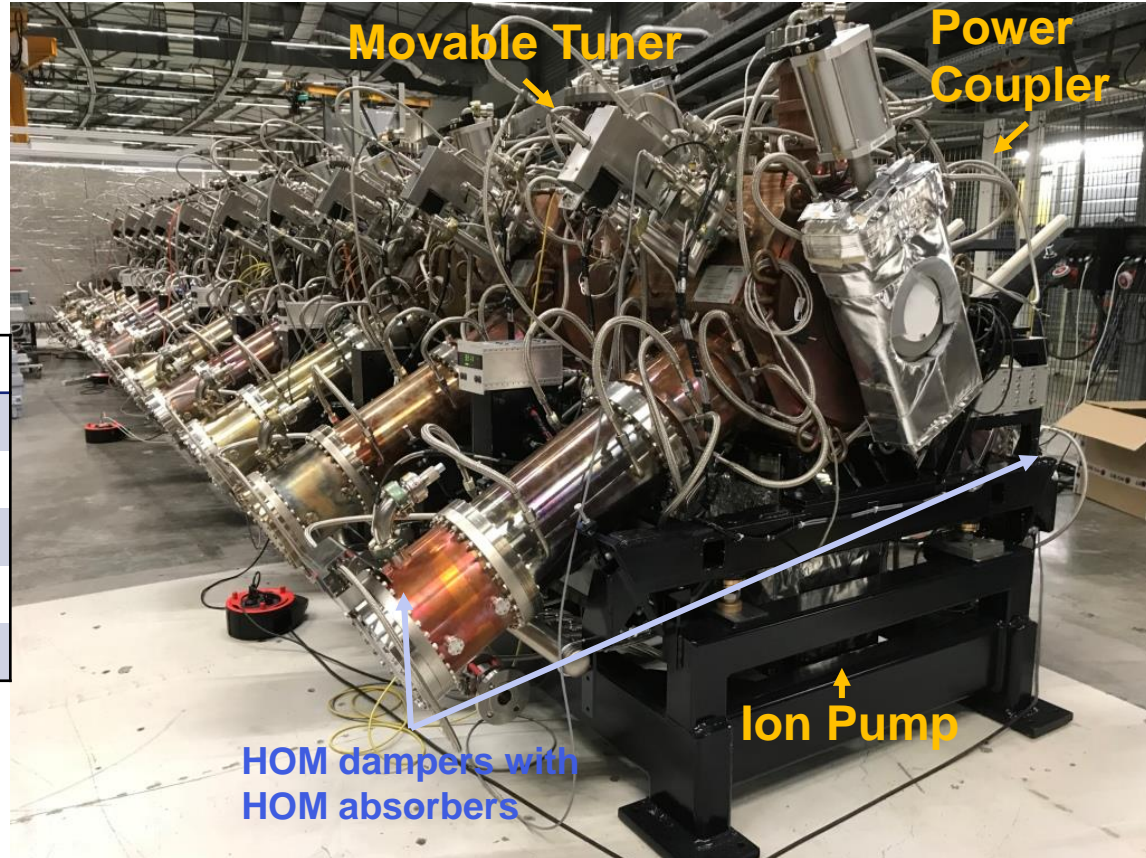
0.75 MV

EBS 30 % less total RF power than now:

≈ 1 MW at nominal 200 mA

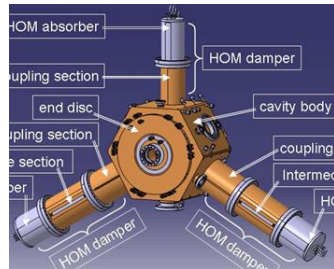
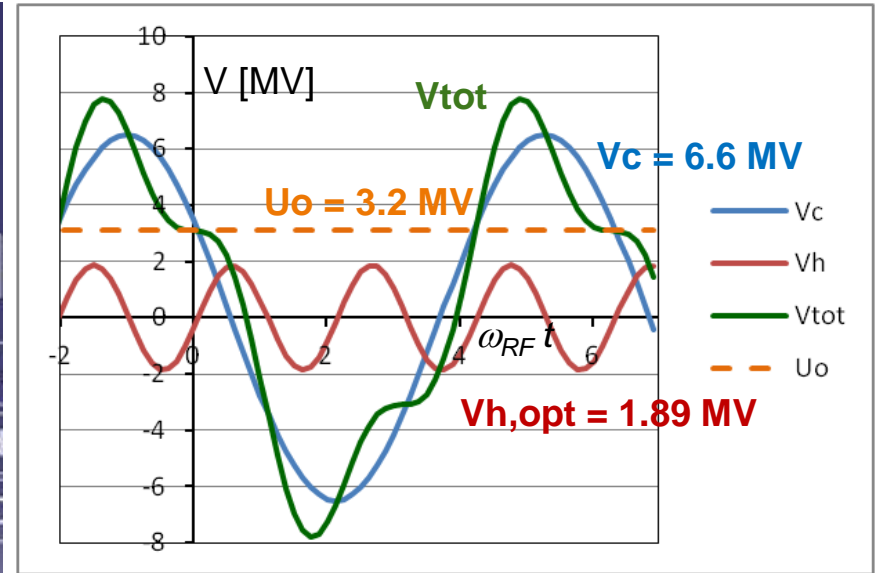
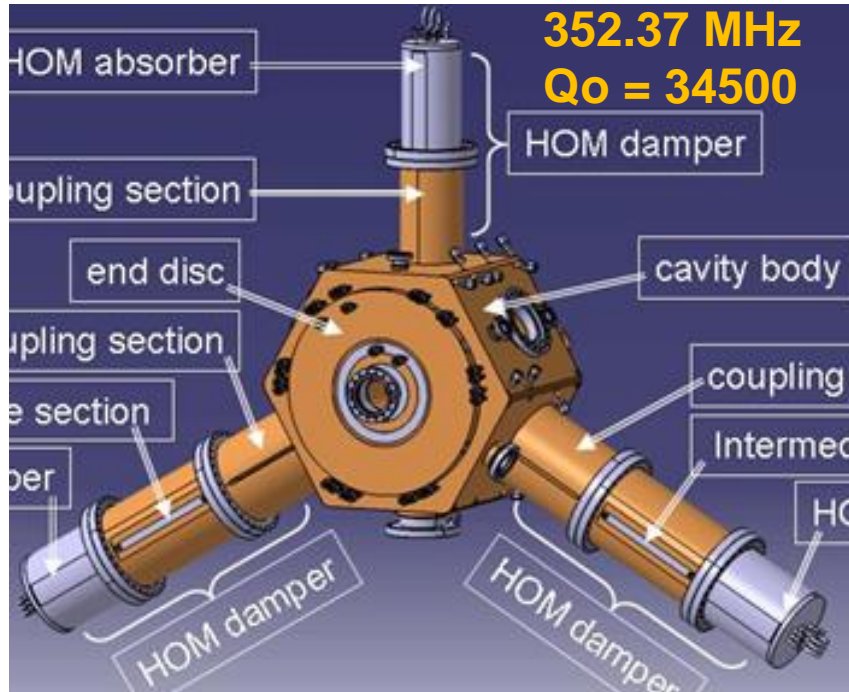
HOM DAMPED SINGLE CELL CAVITIES

f_{res}	352.372	MHz
Q_0	35700	(measured)
R/Q	145	Ω
R_s	≈ 5	M Ω
Tuning range	-350 / +900	kHz
V_{acc} nom/max	500 / 750	kV

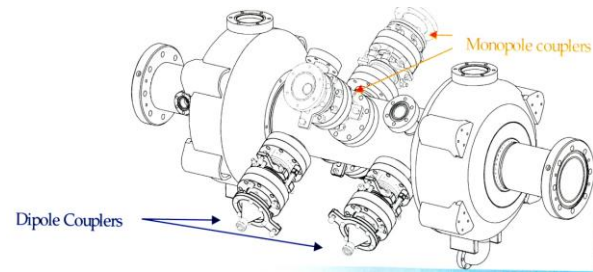


[See A. D'Elia's talk]

HARMONIC RF SYSTEM FOR BUNCH LENGTHENING



Active copper cavity:
Scaling to 1057.1 MHz
 $Q_0 = 20000$
 $R/Q = 145 \Omega$



OR

Passive SC cavity:
Super3HC scaled to 1057.1 MHz

BEAM LOADING - NC ACTIVE HARMONIC CAVITY FOR BUNCH LENGTHENING

$$V_{\text{acc}}(\phi) = V_c \sin(\phi_s + \phi) + V_h \sin(n\phi_h + n\phi)$$

Optimum Working point (1st & 2nd derivatives = 0):

$$\phi_s = \pi - \arcsin[n^2/(n^2-1) U_0/V_c]$$

$$V_{h,\text{opt}} = \text{sqrt}[V_c^2/n^2 - U_0^2/(n^2-1)]$$

$$\phi_{h,\text{opt}} = (1/n) \arcsin[- U_0 / (V_{h,\text{opt}} (n^2-1))]$$

Optimum tuning (min power) \Leftrightarrow load angle = 0:

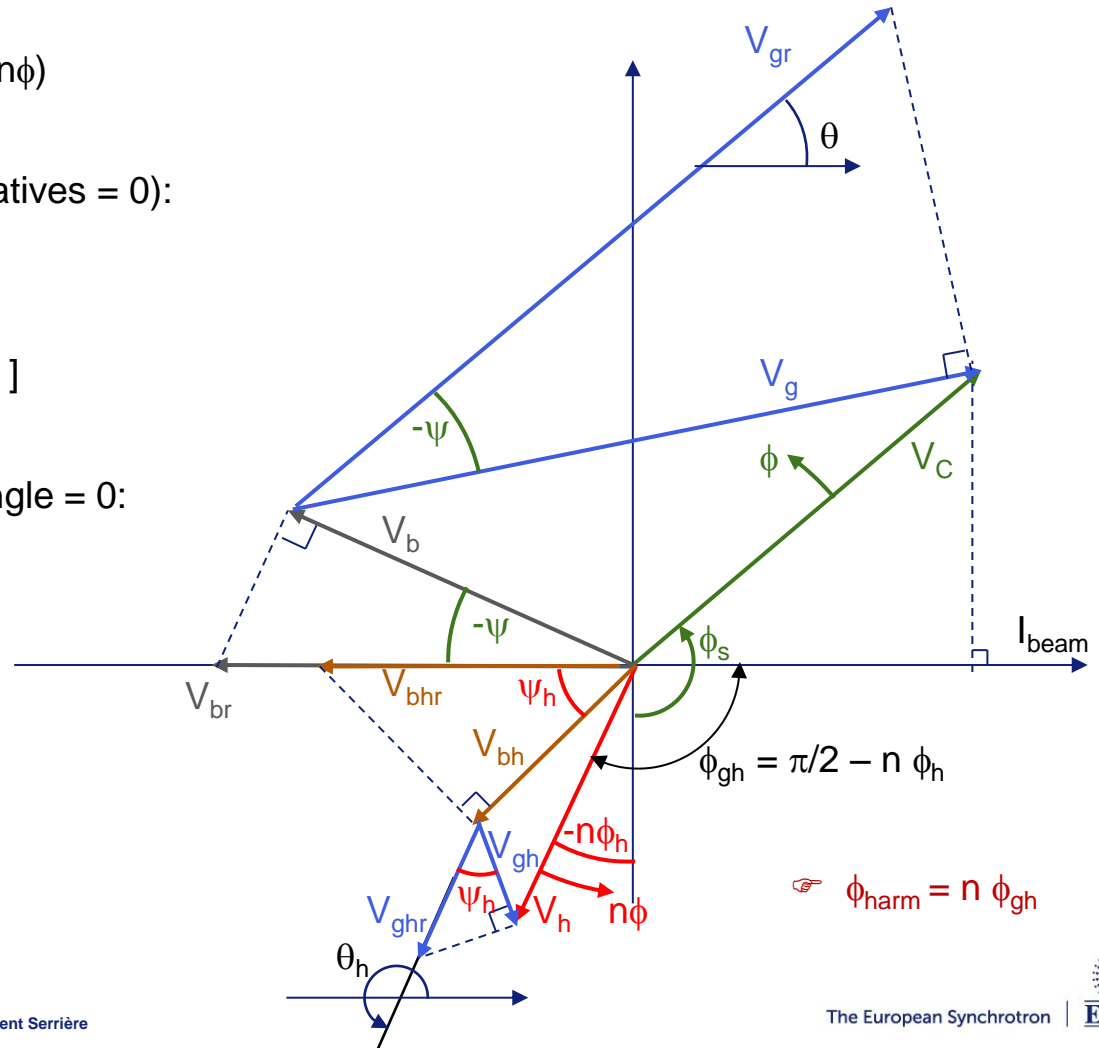
$$\psi \text{ such that } V_{\text{gr}} // V_c$$

$$\psi_h \text{ such that } V_{\text{ghr}} // V_h$$

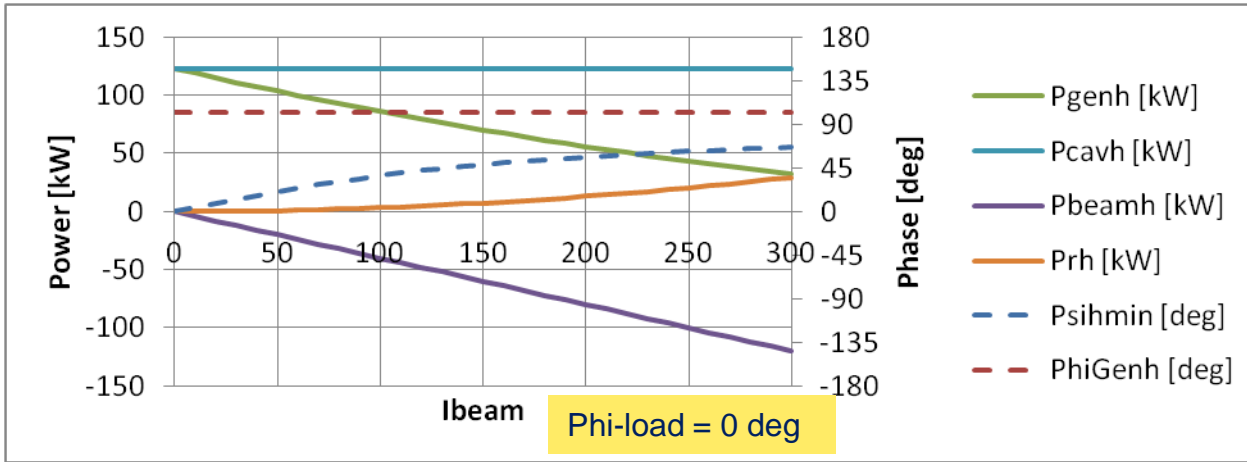
Beware, in the vector diagram:

Main RF turns at $\phi = \omega t$

Harmonic RF at $n\phi = n\omega t$



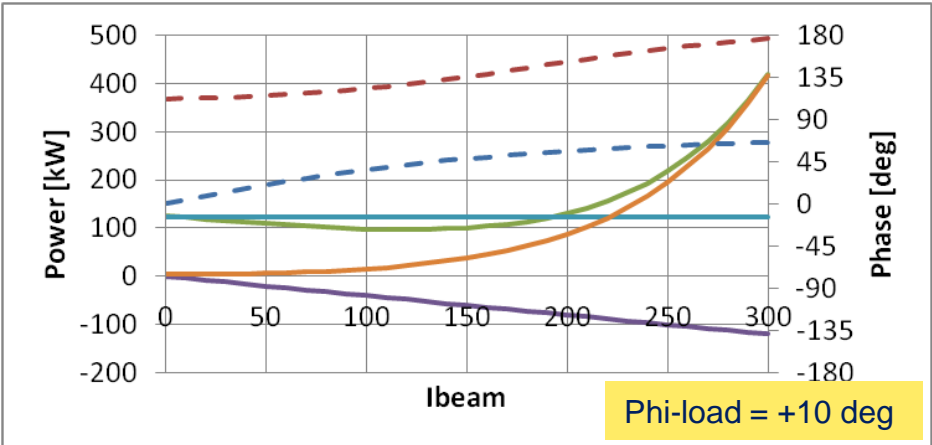
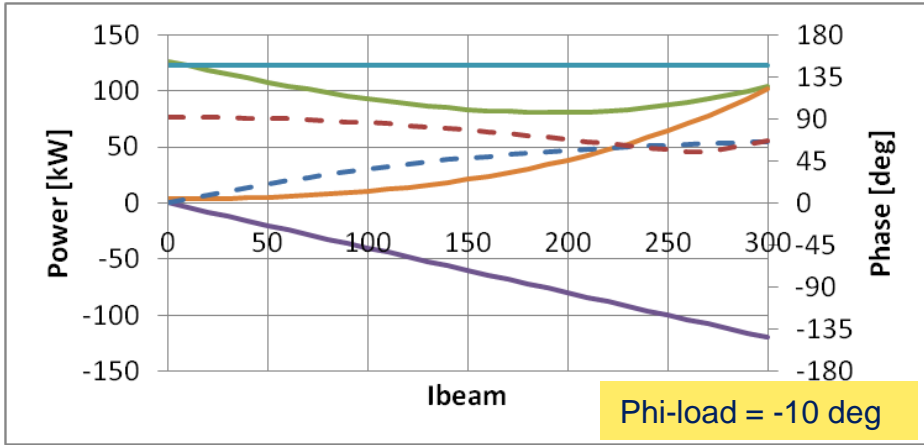
BEAM LOADING FOR FIVE 3RD HARMONIC ACTIVE NC CAVITIES



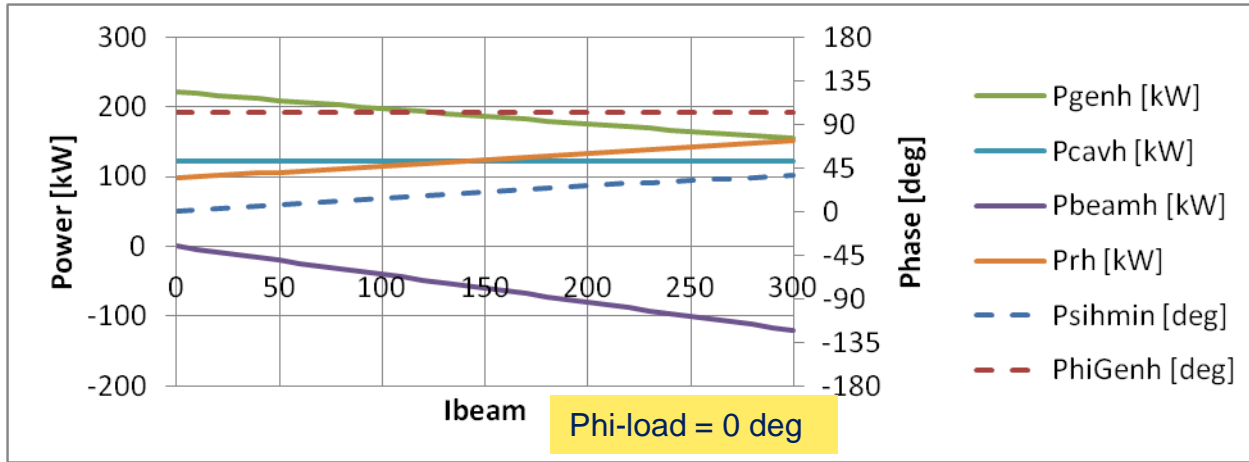
Coupling: $\beta_h = 1$
 $V_h = V_{h,opt} = 1.89$ MV
 $n\phi_h = n\phi_{h,opt} = -12.2$ deg

Working point very sensitive to harmonic cavity tuning

Below 200 mA:
 Pgenh-max = 130 kW



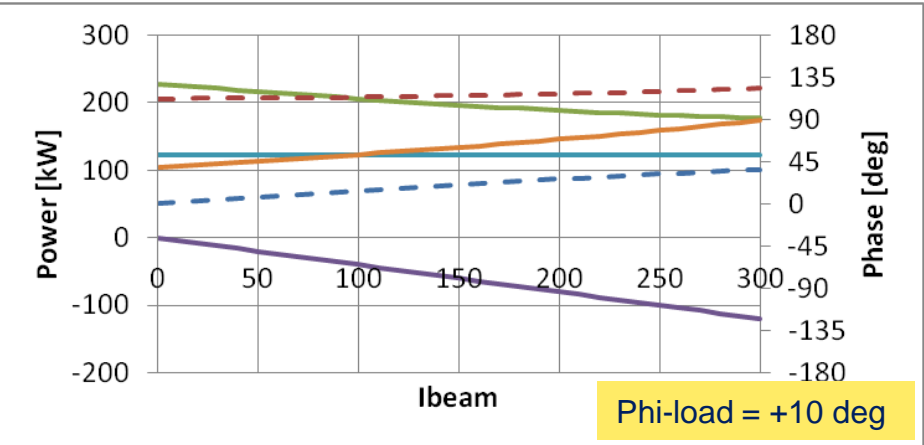
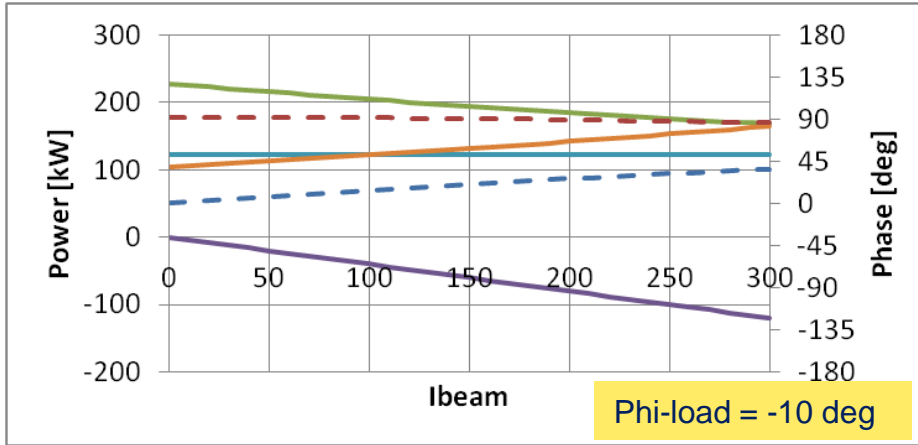
BEAM LOADING FOR FIVE 3RD HARMONIC ACTIVE NC CAVITIES



Coupling: $\beta_h = 5$
 $V_h = V_{h,opt} = 1.89$ MV
 $n\phi_h = n\phi_{h,opt} = -12.2$ deg

Working point less sensitive to harmonic cavity tuning

Below 200 mA:
 $P_{genh-max} = 230$ kW



ROBINSON DC (2ND TYPE) – INTEGRATION OF SYNCHROTRON EQUATION

Assumptions:

RF loops (Amp, Phi, tuning)	slower than	Synchrotron motion	slower than	Cavity Bandwidths (main & HC)
$B \approx 1 \text{ Hz}$	\ll	$f_s \approx 1 \text{ kHz} \dots$	\ll	Above $\approx 40 \text{ kHz}$

1. Tuning angles, generator amplitudes and phases are constant at the scale of the synchrotron motion
2. The beam induced voltages in the cavities follow the beam phase

$$f_s = f_{rf} \times \text{sqrt} [\alpha \mathbf{K}' / (2\pi h E_0/e)], \quad (\mathbf{K}' < 0 \Leftrightarrow \text{DC Robinson instability})$$

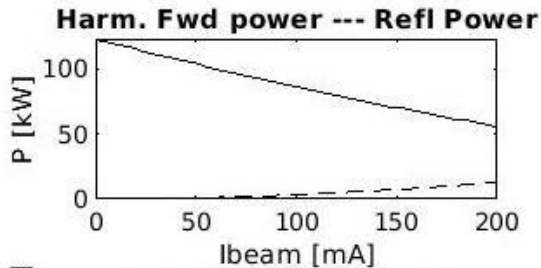
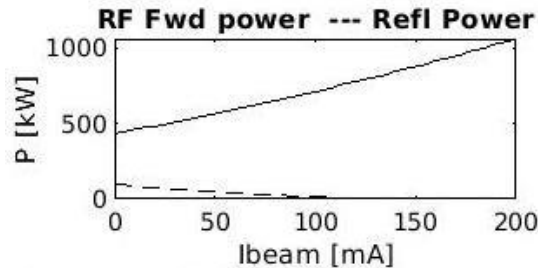
$$\mathbf{K}' = \underbrace{-V_c \cos \phi_s}_{> 0} \underbrace{- nV_h \cos(n\phi_h)}_{< 0} \underbrace{+ V_b \sin \psi}_{< 0} \underbrace{+ nV_{bh} \sin \psi_h}_{> 0} \quad (\text{Eq. 1})$$

Main RF, giving f_{s0}
Harm. RF, for cancelling f_s
Main RF beam loading (Robinson term)
Harm. RF, beam loading (Stabilizing effect)

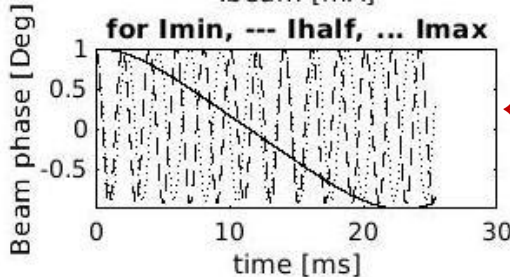
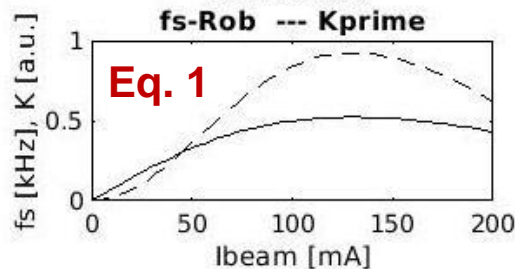
ROBINSON DC (2ND TYPE) – INTEGRATION OF SYNCHROTRON EQUATION

Numerical integration of synchrotron equation:

- Uniform filling (no transients)
- Starting with beam phase offset by +1 or -1 deg
- Tracking V_b , V_{bh} and ϕ_{beam} turn by turn
- Checking convergence (neglecting synchrotron oscillation damping)
- No linearization !

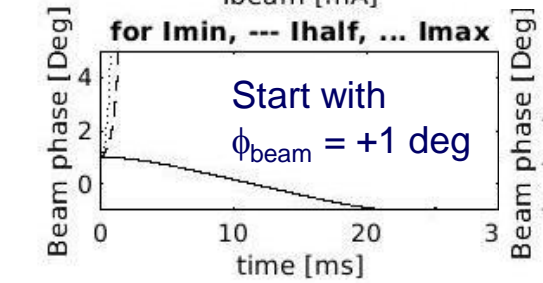
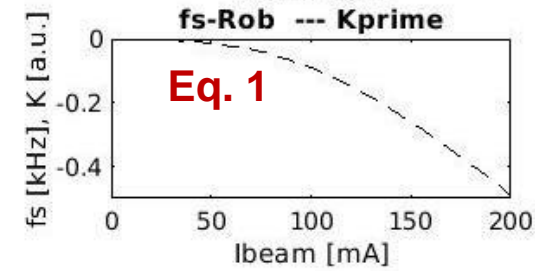
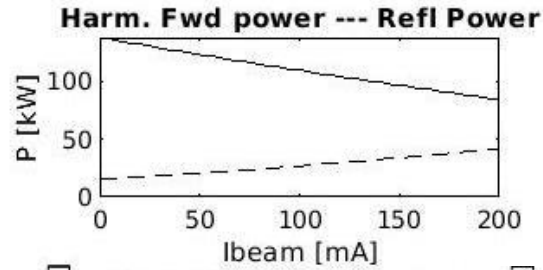
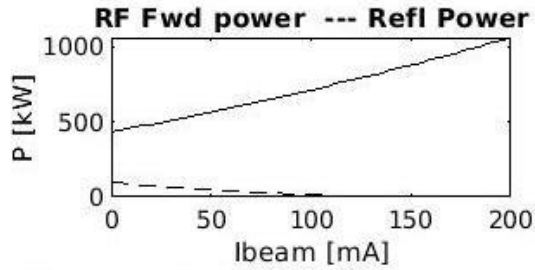


$V_h = V_{h,opt} = 1.89$ MV
 $n\phi_h = n\phi_{h,opt} = -12.2$ deg
5 cavities, $\beta_h = 1$
→ stable

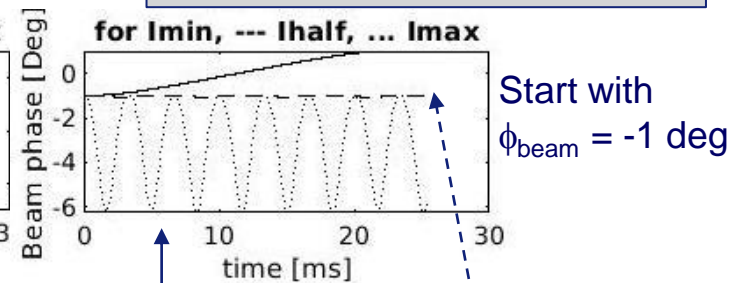


← Numerical integration

ROBINSON DC (2ND TYPE) – INTEGRATION OF SYNCHROTRON EQUATION



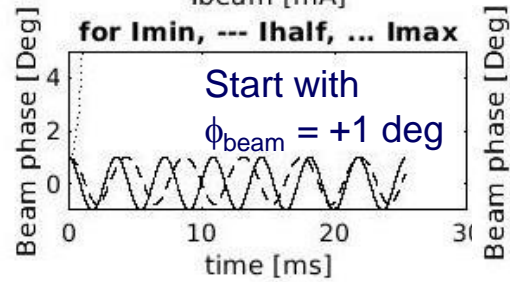
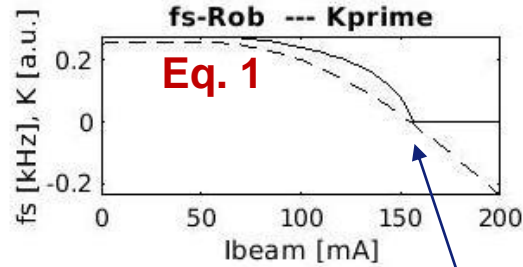
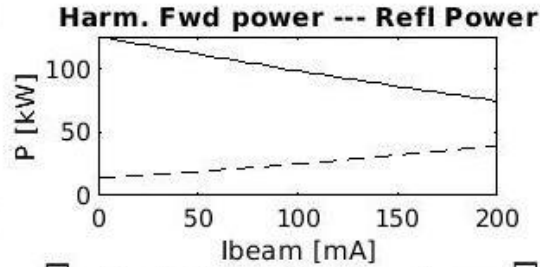
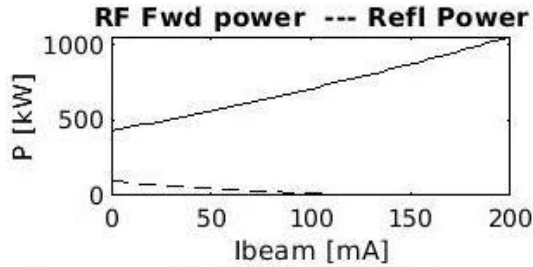
$V_h = V_{h,\text{opt}} = 1.89 \text{ MV}$
 $n\phi_h = n\phi_{h,\text{opt}} = -12.2 \text{ deg}$
 5 cavities, $\beta_h = 2$
 → Unstable for $I_{\text{beam}} > 0$



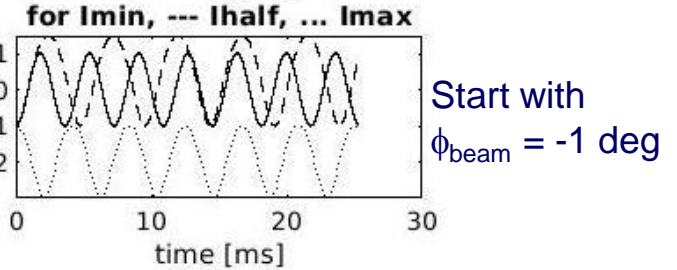
Only for negative beam phases: stabilization through non-linearity of voltage waveform

Equilibrium for $\approx 100 \text{ mA}$

ROBINSON DC (2ND TYPE) – INTEGRATION OF SYNCHROTRON EQUATION

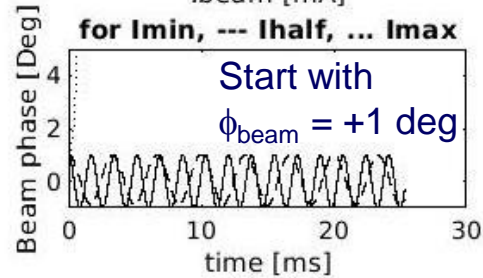
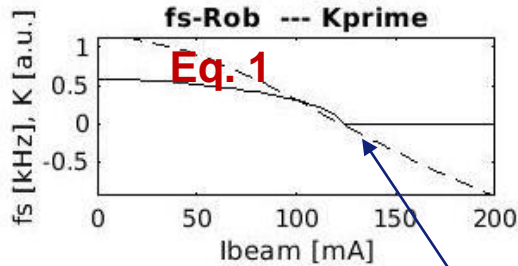
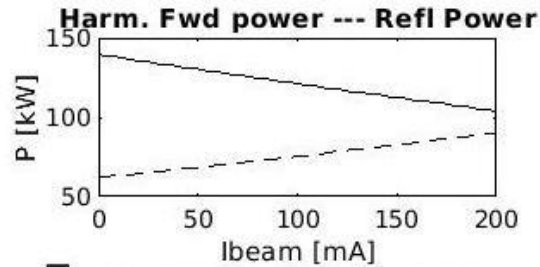
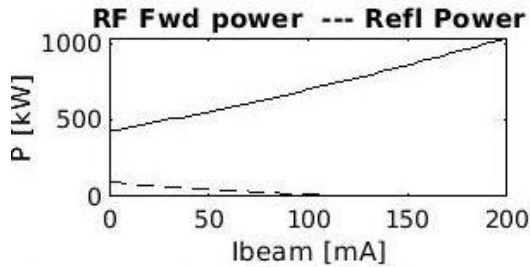


$V_h = 1.80 \text{ MV}$ ($\neq V_{h,\text{opt}}$)
 $n\phi_h = n\phi_{h,\text{opt}} = -12.2 \text{ deg}$
 5 cavities, $\beta_h = 2$
 → Unstable for $I_{\text{beam}} > 150 \text{ mA}$



Threshold at $\approx 150 \text{ mA}$ confirmed by numerical integration

ROBINSON DC (2ND TYPE) – INTEGRATION OF SYNCHROTRON EQUATION



$V_h = 1.50 \text{ MV}$ ($\neq V_{h,opt}$)
 $n\phi_h = n\phi_{h,opt} = -12.2 \text{ deg}$
 5 cavities, $\beta_h = 5$
 \rightarrow Unstable for $I_{beam} > 130 \text{ mA}$

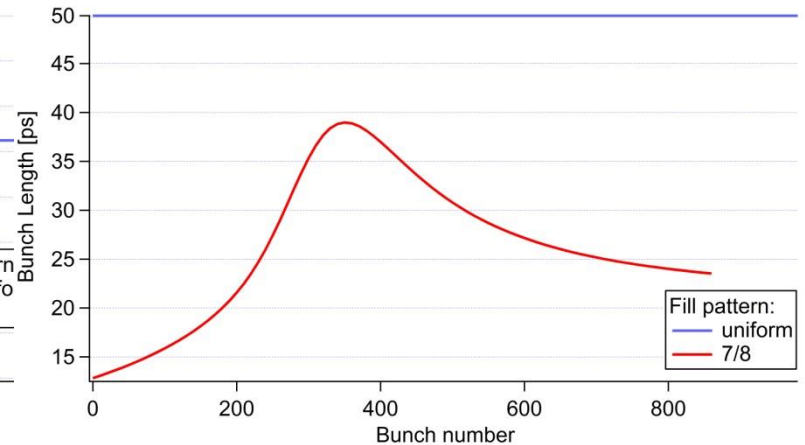
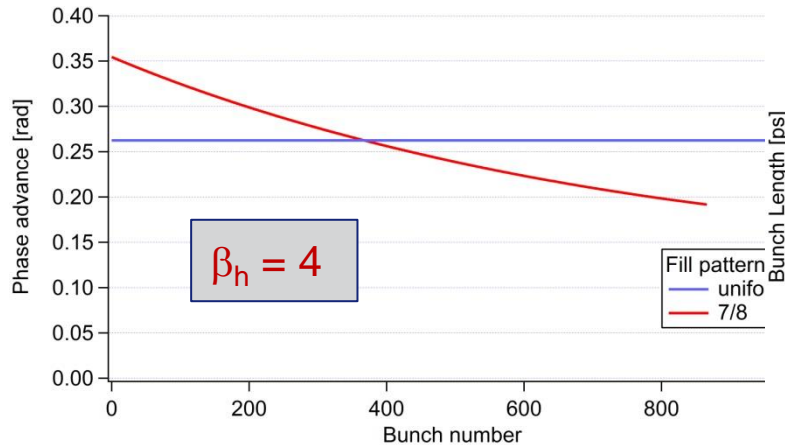
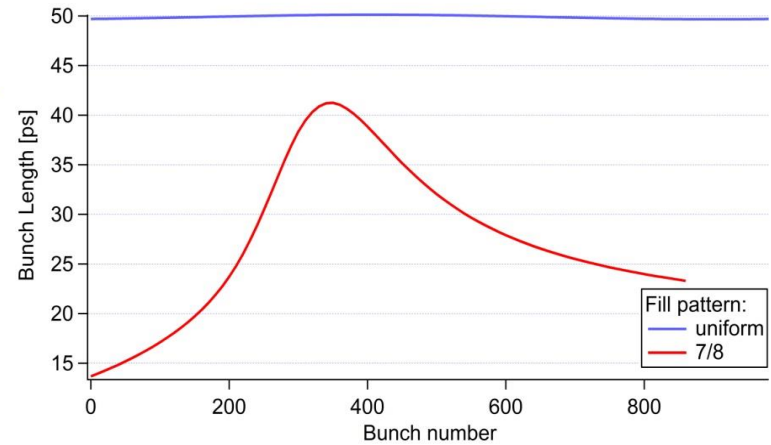
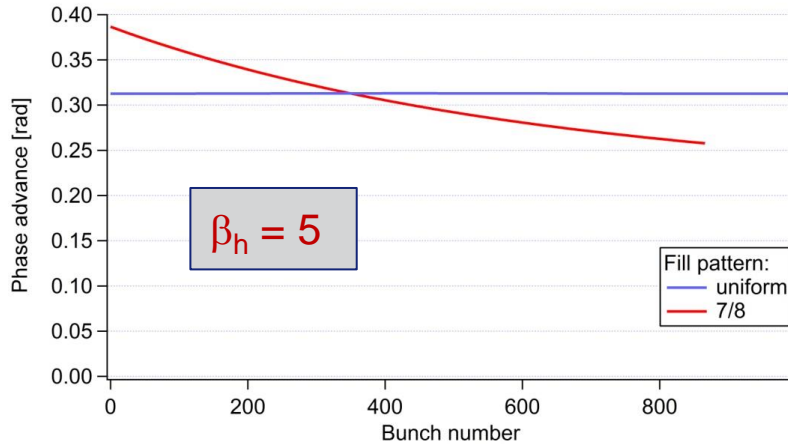
Threshold at $\approx 130 \text{ mA}$ confirmed by numerical integration

For active system, Integration of synchrotron equation indicates:

- **Robinson stable** if Harmonic RF beam loading > Main RF beam loading
 - ⇒ Sufficient harmonic cavity impedance,
 - ⇒ Sufficient number of harmonic cavities
 - ⇒ Upper limit for coupling β_h

MULTIBUNCH / SINGLE PARTICLE TRACKING – ROBINSON & PHASE TRANSIENTS

$V_h = V_{h,opt}$
 $\phi_h = \phi_{h,opt}$
 5 active NC
 cavities



For both cases: Phase transients: 0.16 rad,

! DC Robinson stable for large β_h !

MULTIBUNCH / SINGLE PARTICLE TRACKING – ROBINSON & PHASE TRANSIENTS

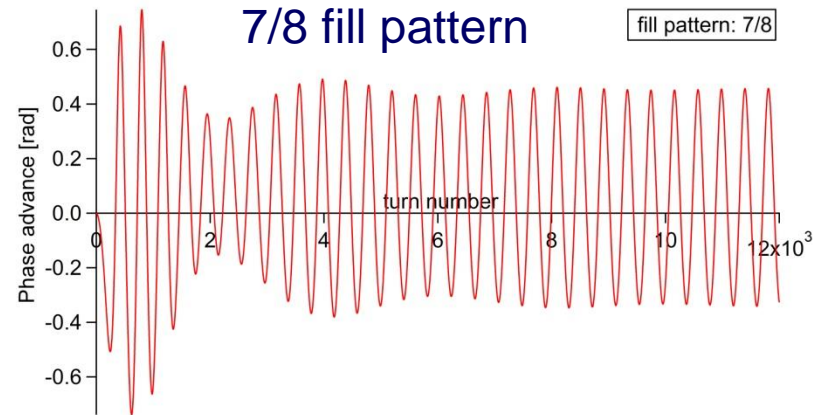
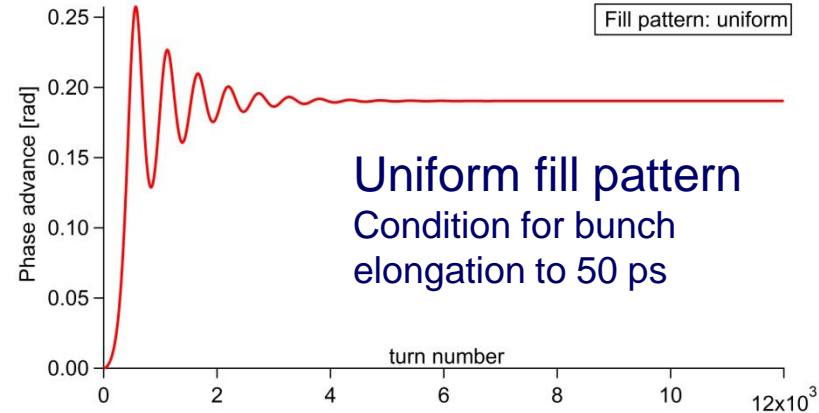
$$V_h = V_{h,opt}$$

$$\phi_h = \phi_{h,opt}$$

5 active NC cavities

$$\beta_h = 3$$

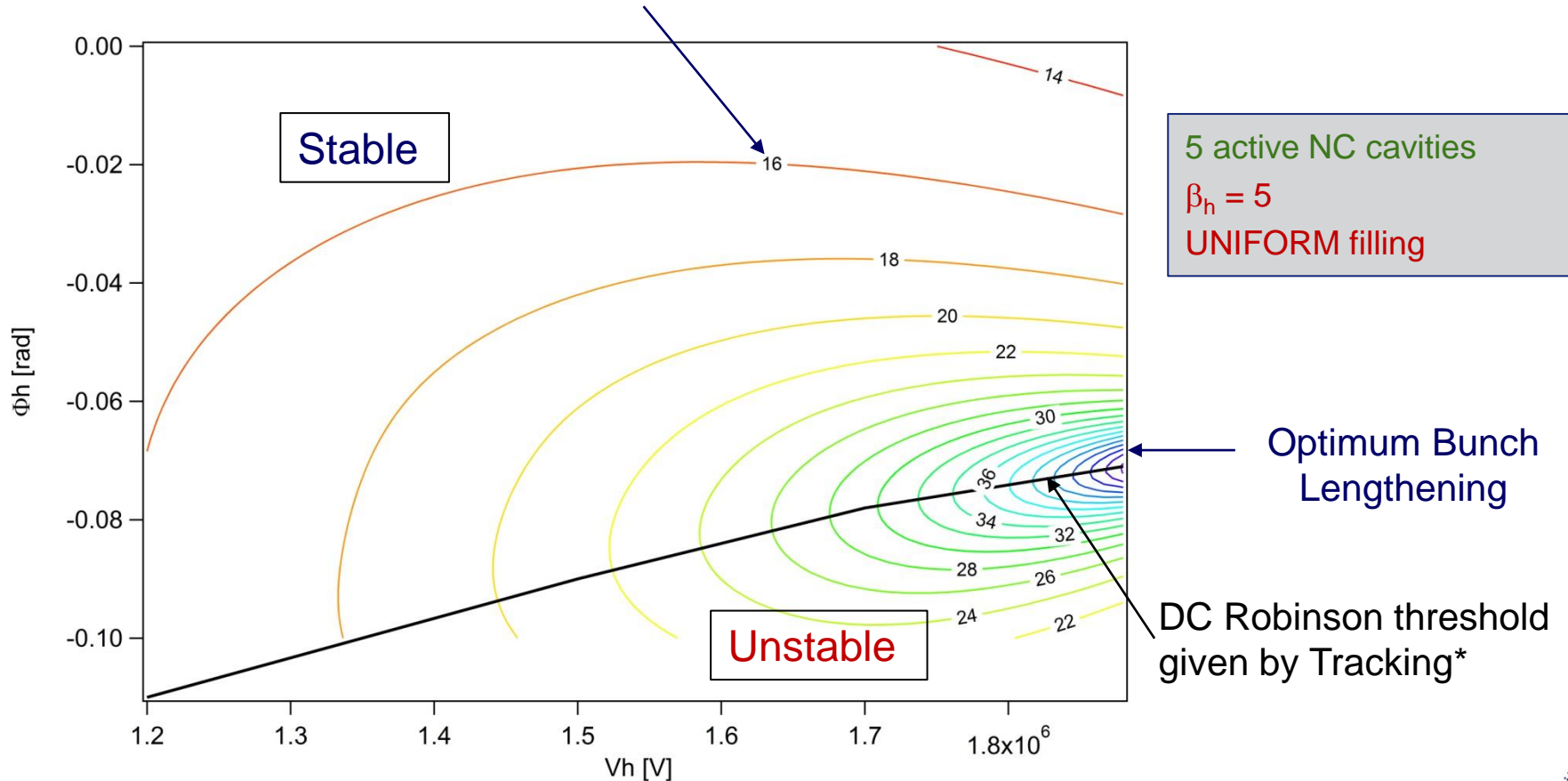
- It looks like AC Robinson instability,
- BUT: needs to be checked with multibunch multiparticle tracking codes !



$\beta_h < 3$: AC like instabilities also for uniform filling

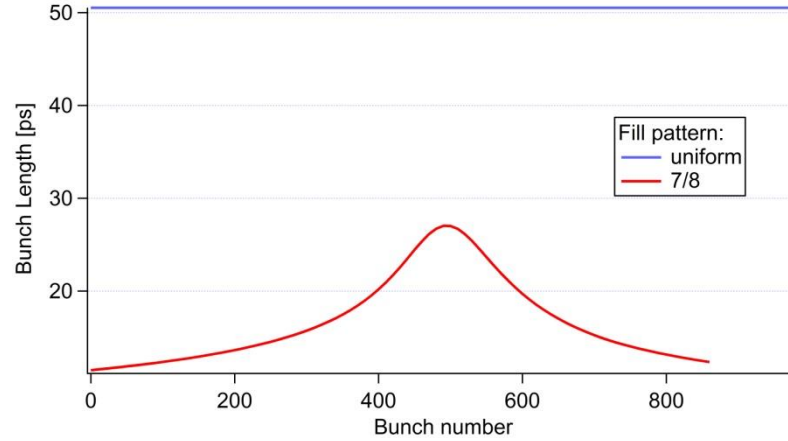
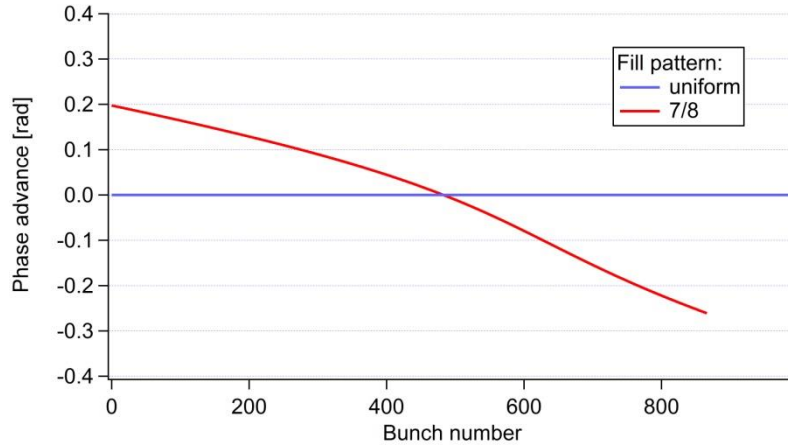
MULTIBUNCH / SINGLE PARTICLE TRACKING – ROBINSON

Bunch length computed with theoretical formula for the obtained total voltage

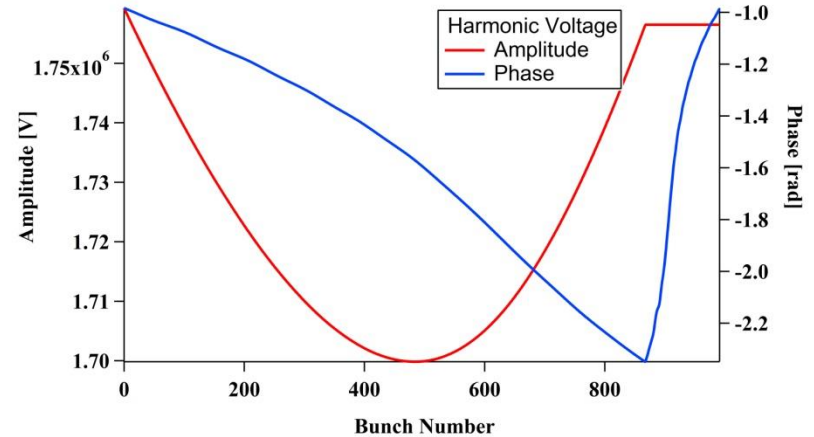


MULTIBUNCH / SINGLE PARTICLE TRACKING – ROBINSON & PHASE TRANSIENTS

Passive SC Cavity: $R/Q = 90 \Omega$, $Q_n = 2e8$



# SC passive Cavities	1	2	3	4	5
Phase Transient [rad]	0.45	0.46	0.54	0.58	0.67



CONCLUSIONS OF THESE VERY PRELIMINARY CALCULATIONS

1. Active normal conducting cavities

- Integration of synchrotron equation indicates that strong beam loading from the harmonic cavities would be needed to avoid Robinson DC
- This is in contradiction with multibunch single particle tracking results requiring high β_h for stability
- Is the obtained AC like instability real? -> to be checked with multiparticle multibunch tracking
- Working points around $[V_{h,opt}, \phi_{h,opt}]$ look close to region of instability: this also needs to be confirmed

2. Passive Super3HC like SC cavities

- Former studies indicate that bunch lengthening operation at low current (e.g. few bunch fillings) is unstable (Robinson AC) unless several SC cavities are installed
- Phase transients with passive harmonic cavities, even with low R/Q as for SC cavities, seem to be stronger than with active cavities: to be confirmed

3. More studies are needed

- The results presented here are very preliminary and partially contradictory
- We decided to show them in order to trigger discussions and motivate further studies